

Fig. 2. $\phi - i$ characteristics of the nonlinear inductor.

Fig. 2 is described as following function.

$$I_k = \frac{\phi_k}{L_2} + \left(\frac{1}{L_1} - \frac{1}{L_2} \right) \frac{|\phi_k + \Phi| - |\phi_k - \Phi|}{2}. \quad (2)$$

By changing the variables and parameters,

$$\begin{aligned} t &= \sqrt{L_1 C} \tau, \quad a = \sqrt[8]{r_d \sqrt{\frac{C}{L_1}}}, \quad \text{“.”} = \frac{d}{d\tau}, \\ \phi_k &= a \sqrt{L_1 C} x_k, \quad i_k = a \sqrt{\frac{C}{L_1}} y_k, \quad v_k = a z_k, \\ \alpha &= \frac{L_1}{L_0}, \quad \beta = r \sqrt{\frac{C}{L_1}}, \quad \gamma = \frac{L_2}{L_0}, \quad \delta = \frac{\Phi}{a \sqrt{L_1 C}}. \end{aligned} \quad (3)$$

the circuit equations are normalized and described as

$$\begin{aligned} \dot{x}_1 &= \frac{1}{1 + m_1 - 2m_1 m_2} \left(\frac{1 - m_1 m_2}{1 - m_1} \{ \beta (X_1 + y_1) - z_1 \} \right. \\ &\quad \left. - \frac{m_1 (1 - m_2)}{1 - m_1} \{ \beta (X_2 + y_2) - z_2 \} \right. \\ &\quad \left. - m_2 \{ \beta (X_3 + y_3) - z_3 \} \right) \end{aligned}$$

$$\begin{aligned} \dot{x}_2 &= \frac{1}{1 + m_1 - 2m_1 m_2} \left(\frac{1 - m_1 m_2}{1 - m_1} \{ \beta (X_2 + y_2) - z_2 \} \right. \\ &\quad \left. - \frac{m_1 (1 - m_2)}{1 - m_1} \{ \beta (X_1 + y_1) - z_1 \} \right. \\ &\quad \left. - m_2 \{ \beta (X_3 + y_3) - z_3 \} \right) \end{aligned}$$

$$\begin{aligned} \dot{x}_3 &= \frac{1}{1 + m_1 - 2m_1 m_2} \left((1 + m_1) \{ \beta (X_3 + y_3) - z_3 \} \right. \\ &\quad \left. - m_1 \{ \beta (X_1 + y_1) - z_1 \} \right. \\ &\quad \left. - m_1 \{ \beta (X_2 + y_2) - z_2 \} \right) \end{aligned}$$

$$\dot{y}_k = \alpha \{ \beta (X_k + y_k) - z_k - f(y_k) \}$$

$$\dot{z}_k = X_k + y_k \quad (k = 1, 2, 3)$$

where

$$X_k = \frac{\alpha}{\gamma} x_k + \left(1 - \frac{\alpha}{\gamma} \right) \frac{|x_k + \delta| - |x_k - \delta|}{2}. \quad (5)$$

$$f(y_k) = \sqrt[3]{y_k}.$$

III. COMPUTER CALCULATED RESULTS

In this section, we perform computer calculations for some cases. First, we consider the case where parameter m_1 is much larger than parameter m_2 . In this case, one subcircuit is not easy to interact with the other subcircuits. Next, the case where parameter m_1 is almost equal to parameter m_2 is considered. All subcircuits dominantly interact in this case. The parameter values corresponding to the inductors are fixed as $\alpha = 20.0$, $\gamma = 10.0$ and (4) is calculated by using the Runge-Kutta method with step size $\Delta t = 0.001$.

A. Case for $m_1 \gg m_2$

We set the parameter values $m_1 = 0.2$ and $m_2 = 0.02$ in this case. Subcircuit 3 is not easy to interact with subcircuits 1 and 2. Therefore subcircuit 3 becomes asynchronous to the others.

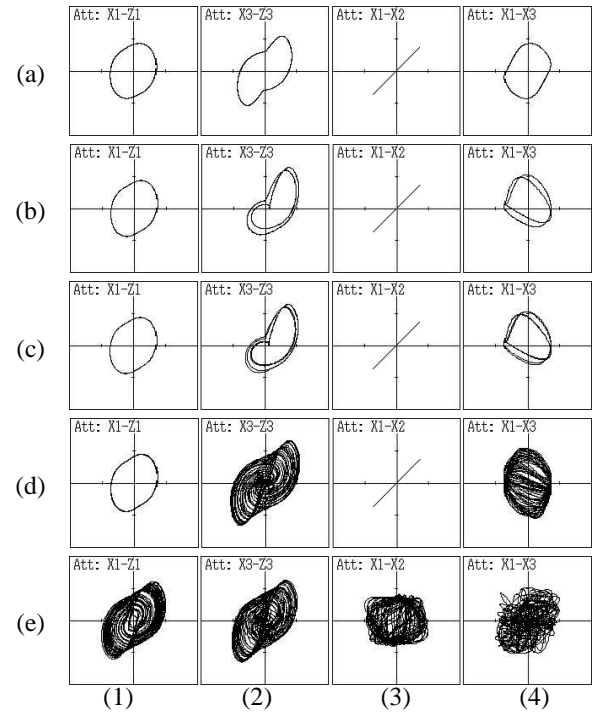


Fig. 3. In-phase synchronization for case A. $m_1 = 0.2$. $m_2 = 0.02$. $\delta = 0.5$. (a) $\beta = 0.15$. (b) $\beta = 0.18$. (c) $\beta = 0.181$. (d) $\beta = 0.2$. (e) $\beta = 0.23$. (1) x_1 vs. z_1 . (2) x_3 vs. z_3 . (3) x_1 vs. x_2 . (4) x_1 vs. x_3 .

Figure 3 shows the in-phase synchronization and the asynchronous state. From Figs. 3(1) and (3), we can confirm that the attractors observed from subcircuit 1 and 2 bifurcate to chaotic attractors keeping in-phase synchronization (a)-(d). While, the attractor observed from subcircuit 3 bifurcates to chaotic attractor via period-doubling route Figs. 3(2)(a)-(e). In

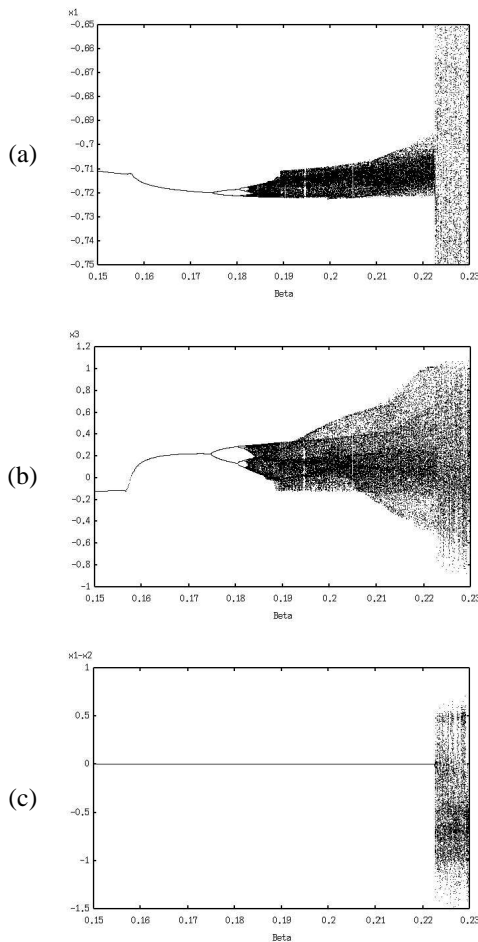


Fig. 4. Bifurcation diagram for the in-phase synchronization. $m_1 = 0.2$. $m_2 = 0.02$. $\delta = 0.5$. (a) Horizontal: β . Vertical: x_1 . (b) Horizontal: β . Vertical: x_3 . (c) Horizontal: β . Vertical: $x_1 - x_2$.

order to investigate the bifurcation route in detail, we made one-parameter bifurcation diagrams. The poincare section is defined as $z_1 = 0, x_1 < 0$. Figure 4 shows the bifurcation diagram for in-phase synchronization. From these figures, we can confirm the bifurcation route via period-doubling. We can also confirm that breakdown of chaos synchronization around $\beta = 0.223$ from Fig. 4(c).

Next, we also investigate the anti-phase synchronization by changing the initial values. Figures 5(a) and (b) shows the anti-phase synchronization for subcircuit 1 and 2. While, the attractors observed from subcircuit 3 become asynchronous state. Figure 6 shows bifurcation diagram for anti-phase synchronization. As parameter β increases, the anti-phase synchronization becomes unstable and the in-phase synchronization is observed around $\beta = 0.2$ as Fig. 5(3)(c) and Fig. 6.

B. Case for $m_1 \approx m_2$

In this case, we set the parameter values $m_1 = 0.2$ and $m_2 = 0.19$. Therefore, subcircuit 3 is easy to interact subcircuit 1 and 2.

First, we investigate the in-phase synchronization. Figure 7 shows that all subcircuits are synchronized at in-phase. How-

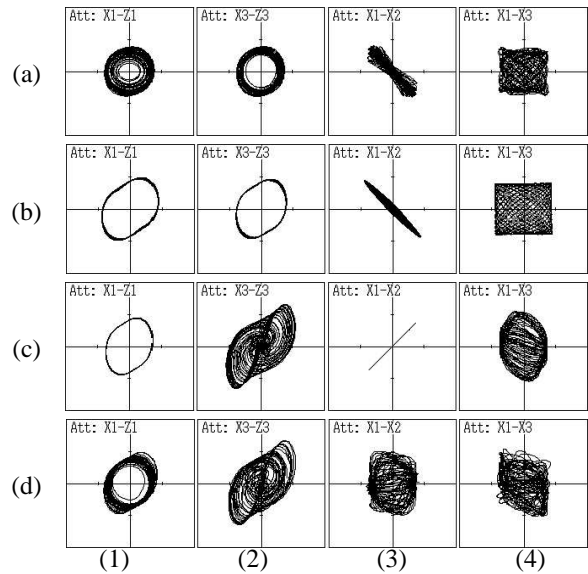


Fig. 5. Anti-phase synchronization for case A. $m_1 = 0.2$. $m_2 = 0.02$. $\delta = 0.5$. (a) $\beta = 0.02$. (b) $\beta = 0.18$. (c) $\beta = 0.2$. (d) $\beta = 0.23$. (1) x_1 vs. z_1 . (2) x_3 vs. z_3 . (3) x_1 vs. x_2 . (4) x_1 vs. x_3 .

ever as β increases, the in-phase synchronization becomes unstable and breaks down (c),(d).

Next, the three-phase synchronization is observed by changing the initial values. Figure 8 shows the three-phase synchronization. From this figure, we can confirm that each one-periodic attractor (a) bifurcates to torus (b), and as β increases, the torus bifurcates to chaos (c) and the chaos grows as (d). Figure 9 shows bifurcation diagram of the three-phase synchronization. We can confirm that the bifurcation route of the three-phase synchronization from Fig. 9, namely bifurcation of the one-periodic solution to torus around $\beta = 0.203$, the generation of chaotic solution for β values more than 0.215 and the generation of periodic solution around $\beta = 0.225$.

IV. CONCLUSIONS

In this research, we investigated quasi-synchronization phenomena observed from simple chaotic circuits with asymmetric coupling by nonlinear mutual inductors. By carrying out the computer calculations, we confirmed that various quasi-synchronization phenomena of chaos were observed.

In the future, we investigate phenomena observed from the case which four or more subcircuit are coupled asymmetrically by nonlinear mutual inductors.

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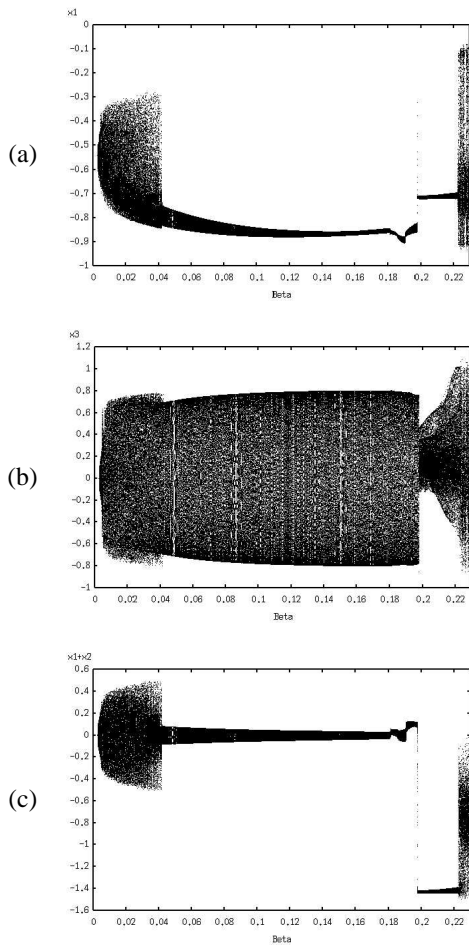


Fig. 6. Bifurcation diagram for the anti-phase synchronization. $m_1 = 0.2$, $m_2 = 0.02$, $\delta = 0.5$. (a) Horizontal: β . Vertical: x_1 . (b) Horizontal: β . Vertical: x_3 . (c) Horizontal: β . Vertical: $x_1 + x_2$.

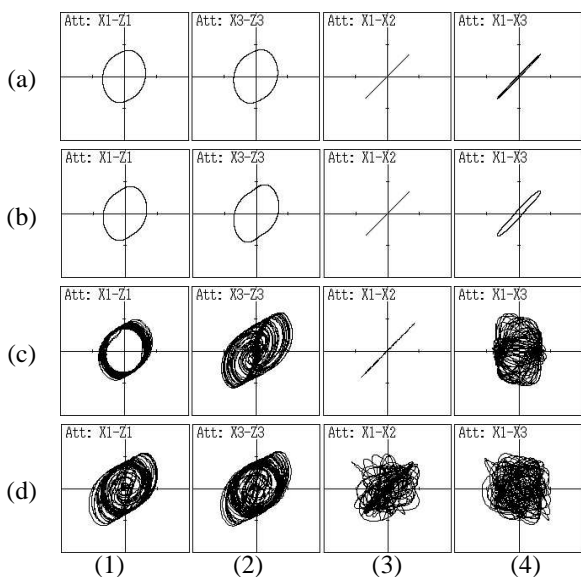


Fig. 7. In-phase synchronization for case B. $m_1 = 0.2$, $m_2 = 0.19$, $\delta = 1.5$. (a) $\beta = 0.15$. (b) $\beta = 0.23$. (c) $\beta = 0.26$. (d) $\beta = 0.27$. (1) x_1 vs. z_1 . (2) x_3 vs. z_3 . (3) x_1 vs. x_2 . (4) x_1 vs. x_3 .

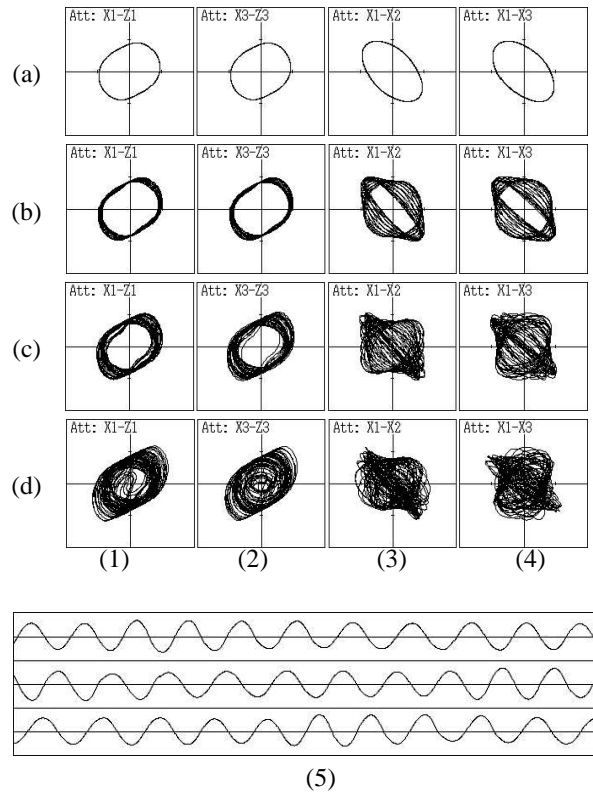


Fig. 8. Three-phase synchronization for case B. $m_1 = 0.2$, $m_2 = 0.19$, $\delta = 1.5$. (a) $\beta = 0.15$. (b) $\beta = 0.2$. (c) $\beta = 0.22$. (d) $\beta = 0.24$. (1) x_1 vs. z_1 . (2) x_3 vs. z_3 . (3) x_1 vs. x_2 . (4) x_1 vs. x_3 . (5) Time waveform for $\beta = 0.22$.

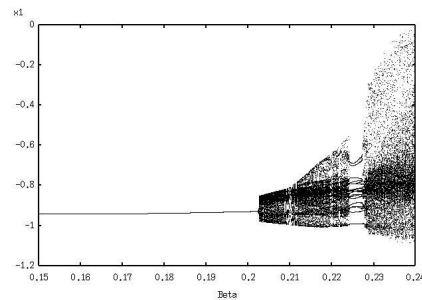


Fig. 9. Bifurcation diagram for the three-phase synchronization. $m_1 = 0.2$, $m_2 = 0.19$, $\delta = 1.5$. Horizontal: β . Vertical: x_1 .

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